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FOR ELECTROMAGNETIC FIELDS

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THIS PAPER WAS PREPARED FOR SUBMITTAL TO
1987 IEEE AP-S INTERNATIONAL SYMPOSIUM
Blacksburg, Virginia
June 15-19, 1987

January 1987

Lawrence
Livermore
National
Laboratory

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RADIATION (ABSORBING) BOUNDARY CONDITIONS * FOR ELECTROMAGNETIC FIELDS

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Introduction

An important problem in finite difference or finite element computation of the electromagnetic field obeying the space-time Maxwell equations with self-consistent sources is that of truncating the outer numerical boundaries properly to avoid spurious numerical reflection. Methods for extrapolating properly the fields just beyond a numerical boundary in free space have been treated by a number of workers. Lindman¹ considered reflection of both propagating and evanescent plane waves at various angles of incidence to a boundary. He used projection operators which process past data at the boundary to update three to six wave equations there. Engquist and Majda² developed a systematic method for "manipulating symbols" to obtain a hierarchy of local boundary conditions at the artificial (truncating) boundaries. They considered 2-dimensional waves impinging on plane boundaries from various directions. Holland³ described a radiation boundary condition for the field scattered from a 3-dimensional object based on an r^{-1} behavior. He observed that a good empirical estimate of "sufficiently large r " was about $d/2$ beyond the scatterer in every direction, d being its largest dimension. This fact motivates our effort to obtain radiation boundary conditions accurate to order $(|r_{\text{source}}|_{\text{max}}/r)^2$. Mur⁴, motivated by the work of Engquist and Majda, manipulated the 3-dimensional scalar wave equation for a radiated field component into a form appropriate for waves at various angles of incidence to a planar boundary. He obtained a second-order finite difference equation which proved to be very efficient for extrapolating tangential \vec{E} just beyond the boundary.

We intend to avoid plane wave assumptions and derive boundary conditions more directly related to the source distribution within the region. We use the Panofsky-Phillips' relations,⁵ which enable one to extrapolate conveniently the vector field components parallel (\parallel) and perpendicular (\perp) to a radial from the coordinate origin chosen near the center of the charge-current distribution.

Analysis

The Panofsky-Phillips equations describe the space-time fields

$$4\pi\sqrt{\epsilon_0/\mu_0} \vec{E}(\vec{r},t) = \vec{e}(\vec{r},t) = \vec{e}_1(\vec{r},t) + \vec{e}_2(\vec{r},t) \quad (1)$$

*This work was performed under the auspices of the U.S. Department of Energy by Lawrence Livermore National Laboratory under contract No. W-7405-Eng-48.

$$4\pi \bar{H}(\bar{r}, t) = \bar{h}(\bar{r}, t) \quad (2)$$

according to volume integrals over retarded sources (in brackets):

$$\bar{e}_1(\bar{r}, t) = c \int \frac{[\rho(\bar{r}', t')]\bar{R}(\bar{r}, \bar{r}')}{R^3} dv' + \int \frac{[\mathbf{J}(\bar{r}', t')]\cdot\bar{R}\bar{R}}{R^4} dv' \quad (3)$$

$$\bar{e}_2(\bar{r}, t) = \int \frac{([\mathbf{J}]\times\bar{R})\times\bar{R}}{R^4} dv' + \frac{1}{c} \int \frac{([\dot{\mathbf{J}}]\times\bar{R})\times\bar{R}}{R^3} dv' \quad (4)$$

$$\bar{h}(\bar{r}, t) = \int \frac{([\mathbf{J}]\times\bar{R})}{R^3} dv' + \frac{1}{c} \int \frac{[\dot{\mathbf{J}}]\times\bar{R}}{R^2} dv' \quad (5)$$

Here the retarded time t' from a retarded source $[\rho]$, $[\mathbf{J}]$, or $[\dot{\mathbf{J}}]$ at \bar{r}' contributing field to the observative space-time point (\bar{r}, t) is

$$t' = t - R/c, \quad R = |\bar{R}| = |\bar{r} - \bar{r}'| \quad (6)$$

The dot denotes $\partial/\partial t'$ at the source or $\partial/\partial t$ at the observation time.

We have applied these equations to extrapolate the fields at point $(\bar{r} + d\bar{r}, t + dt)$ just beyond the numerical boundary in Fig. 1 from those fields at (\bar{r}, t) on the boundary. \bar{r} is a vector from an origin chosen to minimize $|\bar{r}'_{\max}/\bar{r}|^2$. $d\bar{r} = \bar{a}_{||} dr$ is chosen parallel to \bar{r} ; components such as \bar{E}_{\perp} are perpendicular to \bar{r} . The \bar{e}_1 -portion of \bar{e} , consisting of "near-field" in (3), is primarily longitudinal (i.e., parallel to \bar{r}) but has a small transverse component ($\perp \bar{r}$) to be retained. The \bar{e}_2 - and \bar{h} -fields, each of which contains a near-field component $\propto [\mathbf{J}]$ and a "radiation" field component $\propto [\dot{\mathbf{J}}]$, are primarily transverse but have small longitudinal components to be retained.

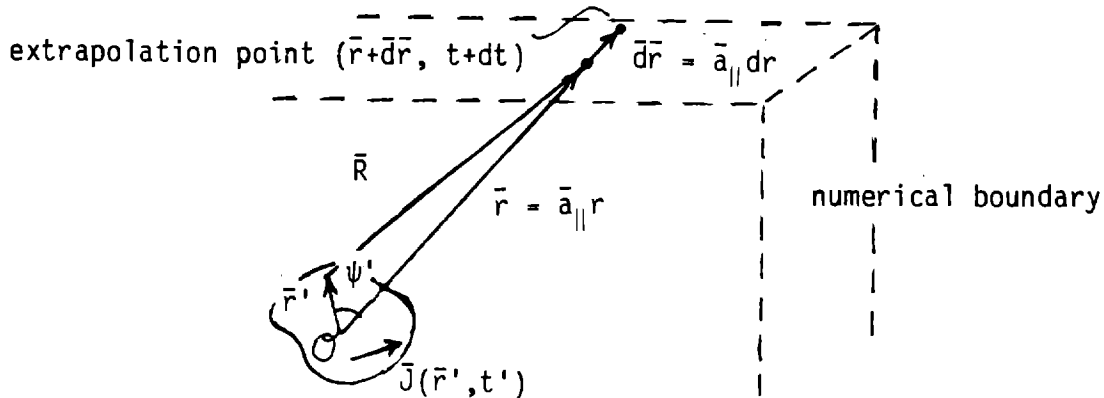


Fig. 1. Geometry for deriving the fields extrapolated to point $(\bar{r} + d\bar{r}, t + dt)$ from those at (\bar{r}, t) from the Panofsky-Phillips relations.

A very convenient property for analysis with \bar{r} fixed is that an arbitrary scalar source $[\rho(\bar{r}', t' = t - R/c)]$ or vector $[J(\bar{r}', t')]$ is unchanged within second order of (r'/r) if (\bar{r}, t) is changed to $(\bar{r} + d\bar{r}, t + dt)$, provided $dt = dr/c$. This implies

$$t' = t - \frac{R(\bar{r}', \bar{r})}{c} = t + dt - R_+(\bar{r}', \bar{r} + d\bar{r})/c, \quad dt = dr/c \quad (7)$$

and follows easily from an expansion of $R(\bar{r}', \bar{r})$:

$$R(\bar{r}', \bar{r}) = [r^2 + (r')^2 - 2rr' \cos \psi']^{1/2} = r \left[1 - \frac{r'}{r} \cos \psi' + \mathcal{O}\left(\frac{r'}{r}\right)^2 \right] \quad (8)$$

Thus

$$R_+(\bar{r}', \bar{r} + d\bar{r}) = r + dr - r' \cos \psi' + \mathcal{O}\left(\frac{r'}{r}\right)^2 \quad (9)$$

and (7) is verified to second-order. Therefore, we may compute changes in the fields (3)-(5) from (\bar{r}, t) to $(\bar{r} + d\bar{r}, t + dt)$ without changing $[\rho]$, $[J]$, or $[J]$ in the integrands!

The results of computing the changes in the fields within second order of (r'/r) are summarized as follows:

$$(\bar{e})_{||}(\bar{r} + d\bar{r}, t + dt) - (\bar{e})_{||}(\bar{r}, t) = d(\bar{e})_{||} = -2 \frac{dr}{r} (\bar{e}(\bar{r}, t))_{||} \quad (10)$$

$$d(\bar{e}_1)_{\perp} = -3 \frac{dr}{r} (\bar{e}_1(\bar{r}, t))_{\perp} \quad (11)$$

$$d(\bar{e}_2)_{\perp} = d(\bar{h})_{\perp} \times \bar{a}_{||} \quad (12)$$

$$d(\bar{h})_{||} = -2 \frac{dr}{r} (\bar{h}(\bar{r}, t))_{||} \quad (13)$$

These depend on the approximations

$$d\bar{R} = d\bar{r} = \bar{R} dr/r = \bar{R}_{||} dr/r, \quad (14)$$

which are made when second-order accuracy can be retained, and

$$\omega R(\bar{r}', \bar{r})/c \gg 1, \quad (15)$$

at all significant frequencies in the sources. This implies the numerical errors will be larger at the lower frequencies.

Equations (10)-(13) suggest a procedure for advancing the field components from (\bar{r}, t) to $(\bar{r} + d\bar{r}, t + dt)$:

- A) Advance $\bar{e}_{||}(\bar{r}, t)$ by $d(\bar{e})_{||}$ according to (10).
- B) Compare the fields at $(\bar{r}-d\bar{r}, t-dt)$ with those at (\bar{r}, t) to obtain the total $d(\bar{e})_{||} = d(\bar{e}_1)_{||} + d(\bar{e}_2)_{||}$ and $d(\bar{h})_{||}$. Use (12) to find $d(\bar{e}_2)_{||}$ and then $d(\bar{e}_1)_{||}$.
- C) Then use (11) to find $(\bar{e}_1(\bar{r}, t))_{||}$, and then $(\bar{e}_2(\bar{r}, t))_{||}$.
- D) With the $(\bar{e})_{||}$ -field thus separated at (\bar{r}, t) , proceed to advance $(\bar{e}_1)_{||}$ and $(\bar{e}_2)_{||}$ to $\bar{r}+d\bar{r}, t+dt$.
- E) If desired, advance $(\bar{h})_{||}$ by (13).

Implementation

We intend to implement this procedure in the finite-difference time-domain code GFDTD for sources within the numerical rectangular parallelopiped in Fig. 1. Since the extrapolation equations are referred to an \bar{r} vector which is generally oblique to the boundary, we must project the field changes--in particular, those of \bar{e} --to a grid of rectangular cells on the boundary. Once the \bar{e} -fields are projected onto the outer edges of finite difference cells at time $t+dt$, they can be used along with the other \bar{e} -field components on edges crossing the boundary and on inside edges to advance \bar{h} on the boundary faces from time $t-dt/2$ to $t+dt/2$ ("leapfrogging" of \bar{e} and \bar{h} in time). If the procedure is efficient, we will compute essentially only the correct outward propagating field from prescribed sources.

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